

**DESCRIPTION OF THE PROGRAM**

**TwoDoFSim\_BB**

**VERSION 1.0**

**May 2013.**

## TABLE OF CONTENTS

### TABLE OF CONTENTS2

#### 1. INTRODUCTION3

**1.1 ABBREVIATIONS:** ..... ERROR! BOOKMARK NOT DEFINED.

**1.2 GENERAL INFORMATION ABOUT PROGRAM** .....3

Purpose and Possibility of the Program..... 3

Short Description..... 3

Limitations..... 4

Standard Conditions ..... 5

#### 2. INPUT DATA AND EXECUTION OF THE PROGRAM5

**2.1 STRUCTURE AND REVIEW OF INPUT DATA**.....5

Projectile data file (PMMdata\_m) ..... 6

**2.2 MODELING INPUT DATA FOR ARTILLERY ROCKETS**.....8

Total Impulse and Burning Time ..... 8

Aerodynamic Drag Coefficient..... 8

**2.1 EXECUTION OF THE PROGRAMS** .....9

Execution of the Main program TwoDoFsim\_BB.m..... 9

Execution of the Program Geom\_InternalBurningTubeWithSlots.m..... 10

#### 4. RESULTS12

**4.1 NUMERICAL RESULTS** ..... 12

**4.2 GRAPHS – DIAGRAMS**.....15

Graphs Generated by Grain Geometry Data File..... 15

Graphs Generated by Main program ..... 16

# 1. INTRODUCTION

## 1.1 GENERAL INFORMATION ABOUT PROGRAM

### Purpose and Possibility of the Program

Capability: Calculation of projectile trajectory and firing elements based on Euler equations of motion for point mass (two degrees of freedom).

Method: Numerical integration of Euler differential equations of motion with two degrees of freedom of projectile and integration of differential equation of burning the propellant.

Purpose of program is quick calculation of trajectory of unguided projectile including firing elements (firing problem solution).

It can also be used for:

- the determination of rocket motor thrust characteristics (total impulse, burning time) for the design of artillery rockets,
- the determination of rocket motor thrust characteristics (total impulse, burning time, optimal ignition time) for the extension of range of classical artillery projectiles and mortar shells,
- the design of the base-bleed unit for the extension of range of classical artillery projectiles,

Motion of projectile is modeled by four differential equations of the first order. Progression of burning area is described by first order differential equation. Equations are solved numerically by fourth order Runge-Kutta method.

Burning area with burning thickness of base-bleed fuel can be entered through specified separate file, or calculated in the program for common geometry.

Program is written in Matlab. It automatically prints all characteristic functions of the process in time and produces graphs.

### Short Description

Program numerically solves (integrates) four differential equations which define flight of projectile for a given initial conditions

$$\frac{dV_K}{dt} = -g \sin \theta \quad (1.1)$$

$$\frac{d\theta}{dt} = -\frac{g}{V_K} \cos \theta \quad (1.2)$$

$$\frac{dx}{dt} = V_K \cos \theta \quad (1.3)$$

$$\frac{dh}{dt} = -V_K \sin \theta \quad (1.4)$$

$$\frac{d\omega_x}{dt} = \frac{L^a}{J_x} \quad (1.5)$$

and differential equation of burning the fuel (propagation of burning area in time)

$$\frac{dy_b}{dt} = r_b \quad (1.6)$$

In the above system of equations independent variable is time  $t$ . The five dependent variables are  $V_K$  (or simple  $V$ ) – projectile velocity,  $\theta (= \gamma)$  – path angle – angle from horizontal line to the velocity vector,  $x$  – range,  $h$  – height from ground,  $\omega_x$  – spin rate,  $L^a$  – aerodynamic rolling moment,  $J_x$  – axial moment of inertia, and  $y_b$  – burning thickness of fuel. Burning rate  $r_b$  depends on pressure in the chamber  $p_c$ , which itself depends on projectile base pressure, and consequently on ambient atmospheric pressure. Pressure in chamber is determined by solving nonlinear equation which defines quasi steady mass flow rate through BB unit opening.

For the meaning of other quantities see lecture supplement and nomenclature in this manual. Initial conditions are defined at launcher muzzle at initial time which is usually taken to be zero:

$$t = 0: \quad V = V_0, \quad \theta = \theta_0, \quad x = x_0 = 0, \quad h = h_0 = 0, \quad y_b = 0.$$

Terminal condition for process in base-bleed unit is defined by maximal burning thickness:

$$y_b = y_{b,\max} : \quad t = t_{y_{b,\max}}.$$

Terminal condition for trajectory is defined by minimum height (impact to ground):

$$h \leq 0: \quad t = t_e.$$

For the integration of system of differential equations the fourth order Runge-Kutta solver is used.

## Limitations

Main limitations of the program are:

- Trajectory is in vertical plane – derivation and deviation due to disturbances cannot be calculated.
- Earth is flat and stationary (Coriolis force is not taken into account).

- Only one propellant with homogeneous characteristics can be considered.
- Burning law of base-bleed fuel is exponential (no free term).

### Standard Conditions

Standard conditions in this software are defined by:

- Standard gravity  $g_{0n} = 9.80665 \text{ m/s}^2$
- Air temperature on MSL  $T_a = 15^\circ\text{C}$
- Atmospheric pressure on MSL  $p_a = 1.013 \text{ bar}$
- Temperature of rocket motor propellant  $T_{p,n} = 20^\circ\text{C}$
- Temperature of base-bleed fuel  $T_{p,f} = 20^\circ\text{C}$

## 2. INPUT DATA AND EXECUTION OF THE PROGRAM

### 2.1 STRUCTURE AND REVIEW OF INPUT DATA

Basically input data are supplied through two input files:

- Grain geometry data file FileName.mat (default file name is ybAbVbAplp.mat)
- Projectile data file FileName.m (default file name is PMMdata\_.m).

Both of them are Matlab files (generated by Matlab).

The relations with notation in theory is given in the following table.

**Table 1 – Grain geometry data file (ybAbVbAplp.mat)**

ybAbVbAplp.mat				
No.	Quantity	Symbol		Description
	in file	in theory	Unit	
1.	y <sub>b</sub>	$y_b$	[m]	Burnt or burning thickness of propellant
2.	A <sub>b</sub>	$A_b$	[m <sup>2</sup> ]	Burning area
3.	BurntVol v <sub>b</sub>	$V_b$	[m <sup>3</sup> ]	Volume of burnt mass
4.	BurntMass m <sub>b</sub>	$m_b$	[kg]	Burnt mass
5.	A <sub>p</sub>	$A_p$	[m <sup>2</sup> ]	Port area
6.	l <sub>p</sub>	$l_p$	[m]	Port perimeter

User can generate that file either by using analytical formulas or by any 3D solid modeler CAD program (SolidWorks, AutoCAD, CATIA ...) and transfer to Matlab and make grain geometry data file. In both cases finally it should be made in Matlab in order to be written in **.mat** format.

### Projectile data file (PMMdata\_.m)

File contains necessary data to calculate trajectory and process in base-bleed unit.

**Table 2 – Projectile data file (PMMdata\_.m)**

PMMdata_.m				
No.	Quantity	Symbol		Description
	in file	in theory	Unit	
1.	clc;	–	–	Matlab statement – clears Matlab work space
2.	close all;	–	–	Matlab statement – Closes all Matlab opened figures
3.	Title	–	–	Identifier of weapon/projectile. It serves as information purposes – not significant for calculation. It is printed in work space.
4.	dref	$d$	[m]	Reference length - calibre
5.	Sref	$S$	[m <sup>2</sup> ]	Reference area. Usually $S = d^2\pi/4$
6.	mass0	$m_0$	[kg]	Projectile initial mass
7.	twistd	$\varphi$	[deg]	Barrel rifling twist angle
8.	Jx0	$m_0$	[kgm <sup>2</sup> ]	Projectile initial moment of inertia
9.	iet	$i_{et}$	[-]	Drag form factor - correction factor for drag coefficient. For the example in this report (Rdz_Fr_155mm) $i_{et} = 1$ , because coded drag coefficient is calculated exactly for the projectile considered in the example. For any other shape of projectile, or any other coded drag coefficient drag form coefficient should be determined to achieve range obtained by experiment. See also section “Coding the Aerodynamic Coefficients” in this report and corresponding LS.
10.	IdentRM	–	[-]	RM operation On/Off identifier. For IdentRM=0 operation of rocket motor is off.. For IdentRM=1 operation of rocket motor is on.
11.	Itot	$I_T, I_{tot}$	[Ns]	Total impulse of RM
12.	propmass	$m_p$	[kg]	Propellant mass of RM
13.	tburn	$t_b$	[s]	Burning time of RM
14.	tign	$t_{ign}$	[s]	Ignition time of RM
15.	IdentBB	–	[-]	BB operation On/Off identifier. For IdentBB=0 operation of rocket motor is off.. For IdentBB=1 operation of rocket motor is on.
16.	tignBB	$t_{i, BB}$	[s]	Ignition time of BB
17.	dbase	$d_b$	[m]	Base diameter of projectile – base diameter of BB unit
18.	Sbase	$S_b$	[m <sup>2</sup> ]	Base area, $S_b = d_b^2\pi/4$

19.	rhof	$\rho_f$	[kg/m <sup>3</sup> ]	Density of BB fuel
20.	Lp	$L_p$	[m]	Length of BB grain of BB grain
21.	Ns	$N_s$	[-]	Number of slots of BB grain
22.	Dp	$D_p$	[m]	Diameter (outer) of grain of BB fuel
23.	Di	$D_i$	[m]	Inner diameter of BB grain
24.	bs	$b_s$	[m]	Slot width of BB grain
25.	dm	$d_m$	[m]	Diameter of cylindrical part with nozzle. This diameter exists when BB unit is around the RM nozzle. For the design case with no RM $d_m = 0$ .
26.	Ae	$A_e$	m <sup>2</sup>	Opening (exit) area
27.	Geom_File()	–	–	Name of file which generates file ybAbVbAplp.mat which contains geometrical characteristics of BB grain and burning geometry with respect to burning thickness. In this example file name is Geom_InternalBurningTubeWithSlots (); See Grain Geometry Data File section. The file can be disabled by inserting character % before the file name. Than file ybAbVbAplp.mat is not generated by running the file, but it may be generated by earlier run of this file, or it can be generated upon the running any other program.
28.	Rgas	$R$	[J/kgK]	Gas (specific) constant of BB burning product. In this program it is assumed that it is independent of pressure in the chamber.
29.	Tflame	$T_f$	[K]	Adiabatic flame temperature of BB fuel. In this program it is assumed that it is independent of pressure in the chamber.
30.	kappa	$\kappa$	–	Ratio of specific heats. In this program it is assumed that it is independent of pressure in the chamber.
31.	etath	$\eta_\theta$	–	Coefficient of thermal reduction. It is assumed that mean temperature in chamber is less than flame temperature by amount defined by this coefficient, so that $T_c = \eta_\theta T_f$ . Practical values for the coefficient are $\eta_\theta = 0.985 \div 0.995$ . The coefficient is not implemented in this version – it will be implemented in the next version.
32.	cetad	$\zeta_d$	–	Coefficient of discharge efficiency. It is assumed that discharge mass flow rate is less than theoretical one by amount defined by this coefficient, so that $\dot{m}_e = \zeta_d \dot{m}_{e,theor}$ . Practical values for the coefficient are $\eta_\theta = 0.980 \div 0.995$ . The coefficient is not implemented in this version – it will be implemented in the next version.
33.	brb	$b$	[m/s]	Coefficient in burning rate law defined by $r_b = b p_c^n$ for standard BB fuel temperature $T_{p,f} = 21^\circ\text{C}$ and stationary BB unit (non-accelerated, non-spinning propellant). Note that value of coefficient is for pressure is in Pascals.
34.	nrb	$n$	–	Exponent in burning rate law defined by $r_b = b p_c^n$ . The value ranges from 0 to 1 depending of propellant composition. Note that higher values than 1 generate unstable burning process in chamber.
35.	k1p	$k_1$	–	Coefficient of the influence of spin rate on burning rate $r_b = k_1 b p_c^n$ of BB fuel. It depends on spin rate and of fuel composition. The value ranges from 1.1 to 1.2 for typical spin stabilized projectiles,

				but user can enter experimentally determined value for corresponding spin rate. Note that spin vs. time is calculated in the program and can be used for coding function $k_1 = f(\omega_x)$ , $\omega_x$ being spin rate (pspin).
36.	betarb	$\beta$	[1/K]	Coefficient of the influence of propellant temperature on burning rate $r_b = e^{\beta(T_p - T_{p,n})} k_1 b p_c^n$ . The value ranges from 0.0012 to 0.0016 depending of propellant composition. The coefficient is not implemented in this version – it will be implemented in the next version.
37.	Ta0c	$T_{a0}$	[°C]	Ground air temperature
38.	pa0	$p_{a0}$	[mbar]	Ground air pressure
39.	Windx	$W_x$	[m/s]	Ground longitudinal wind. Positive value is in the direction of flight (tail wind). Negative value is in opposite direction of flight (head wind).
40.	v0	$V_0$	[m/s]	Muzzle velocity - Projectile initial velocity with respect to ground. It should be greater than zero.
41.	iTheta0d	$\theta_{0i}$	[deg]	Initial elevation angle, $\theta_{0i} > 0$
42.	dTheta0d	$d\theta_0$	[deg]	Increment of elevation angle
43.	NTheta0d	$n_{\theta_0}$	[-]	Number of elevation angles
44.	Ts	$T_s$	[s]	Integration step for solving system of differential equations which define process in RM. To large integration step can produce instability in integration. It is recommended to choose 100ms at start and carefully increase the value preserving desired accuracy
45.	jprint	-	-	Printing step ratio – ratio of the printing step and integration step. It is always greater than unity. For example, to print each tenth point obtain by integration, put jprint=10
46.	PrintToFileID	-	-	Output file Identifier. PrintToFileID=0 – Results printed to Matlab Workspace; PrintToFileID=1 – Results printed to file PPMResults.txt;

## 2.2 MODELING INPUT DATA FOR ARTILLERY ROCKETS

### Total Impulse and Burning Time

Program does not calculate motion of projectile in barrel or on the launcher. The initial velocity should be greater than zero. For artillery rocket user ought to enter muzzle velocity as for the artillery shells. For this reason total impulse of the rocket motor for the remaining of flight should be reduce for the amount consumed to boost rocket to muzzle velocity.

### Aerodynamic Drag Coefficient

Aerodynamic drag coefficient is coded in the program (see section “Coding the Aerodynamic

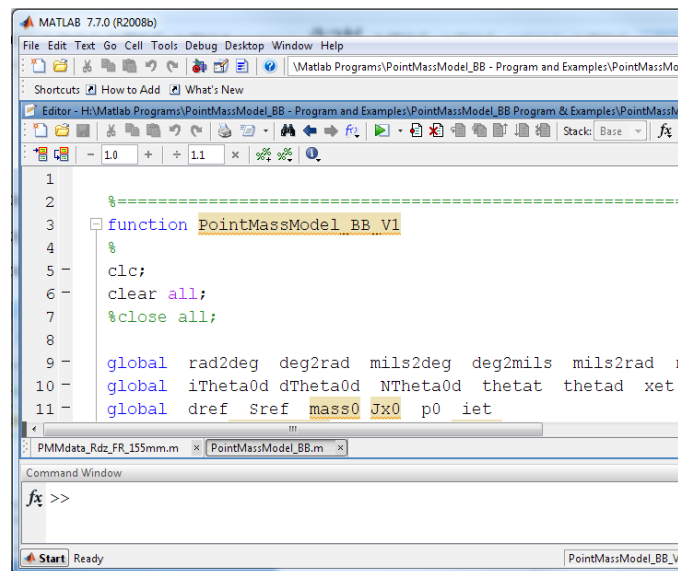


Coefficients”). For spin stabilized projectiles it is suggested to use  $C_{D.43}$  etalon coefficient. For fin stabilized projectiles  $C_{D.58}$  etalon coefficient is more appropriate (see LS “Basis of External Ballistics - Point Mass Model”). Based on used chosen drag coefficient, drag form factor is to be determined from firing, or from firing tables.

## 2.1 EXECUTION OF THE PROGRAMS

### Execution of the Main program TwoDoFsim\_BB.m

To run the main program double click on TwoDoFsim\_BB.m. The main program window appears. Or, alternatively run Matlab program first and open the file TwoDoFsim\_BB.m. In both cases Matlab environment should be opened.



```

1
2
3 function PointMassModel_BB_V1
4
5 clc;
6 clear all;
7 %close all;
8
9 global rad2deg deg2rad mils2deg deg2mils mils2rad r
10 global iTheta0d gTheta0d NTheta0d thetat thetad xet
11 global dref Sref mass0 Jx0 p0 iet

```

Figure – Matlab environment and main program.

Upon the running of the program the following dialog appears for opening/running file with projectile data,

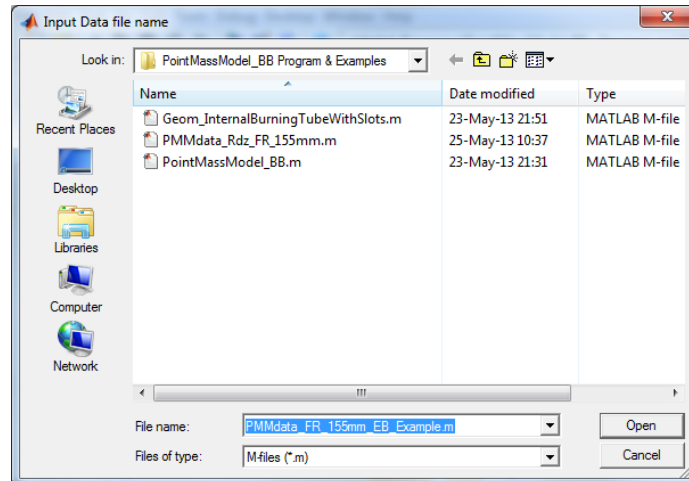


Figure – Dialog for opening file with rocket motor data.

And, after that, dialog for opening/running file with grain geometry data appears.

User can search any directory and choose any appropriate data. Note that default offered file `ybAbVbAplp.mat` is generated by program `Geom_File` (`Geom_InternalBurningTubeWithSlots.m` in this example) called in `PMMdata_.m` file (`PMMdata_Rdz_FR_155mm.m` in this example).

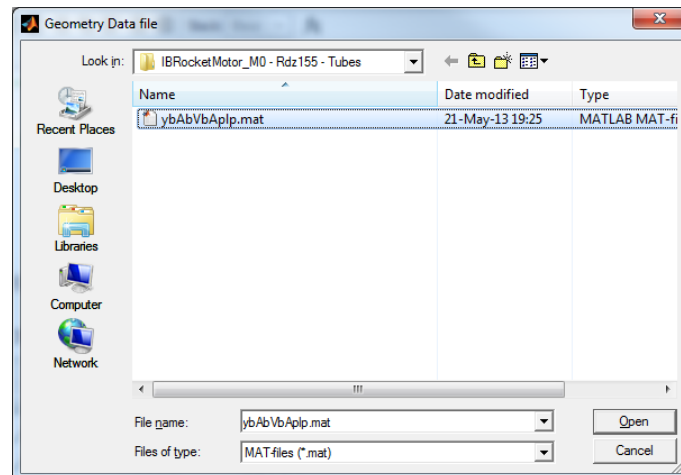


Figure – Dialog for opening file with grain geometry data.

### Execution of the Program `Geom_InternalBurningTubeWithSlots.m`

The Program (function)

```
Geom_InternalBurningTubeWithSlots(Lp,Ns,Dp,Di,bs,rhop,PrintID,PlotID);
```

which is used for generating the geometry data, can be called on two ways: with arguments (like above) and without arguments – geometrical parameters. When it is called with arguments it uses arguments which are passed to function. When it is called without

arguments it uses geometrical parameters coded in the body of function. For example calling by statement (no arguments)

```
Geom_InternalBurningTubeWithSlots();
```

effects in using the parameters coded in function body

```

=====
function Geom_InternalBurningTubeWithSlots(Lp,Ns,Dp,Di,bs,rhop,PrintID,PlotID);
% calculation of burning area for internal-Burning Tube with slots
% Side surfaces and outer surface are inhibited.

% Note:  Dimensions in [m]

clc;
%clear all;
%close all;
%-----
if nargin == 0      % If number of input arguments is zero use the following
                   % values for grain characteristics
    Lp      = 100.0e-3;      % m      Length
    Ns      = 3;           % -      Number of slots
    Dp      = 116.7e-3;     % m      Outer diameter of the grain
    Di      = 60.0e-3;     % m      Inner diameter of the grain
    bs      = 3.0e-3;      % m      Slot width
    web     = 0.5 * (Dp - Di); % m      Web
    rhop    = 1598;        % kg/m3 Density
    PrintID = 1;          % Printing identifier;
                                % PrintID=0 - No printing,
                                % PrintID=1 - Printed in work space
    PlotID  = 1;          % Plotting identifier;
                                % PlotID=0 - No plotting,
                                % PlotID=1 - Graphs are plotted
end;
%-----
%
%
...

```

## 4. RESULTS

### 4.1 NUMERICAL RESULTS

Upon the successful run of the program results are printed in workspace. Here is an example of eight trajectories ( $i\text{Theta}0d=42.5$ ,  $N\text{Theta}0d=8$ ,  $d\text{Theta}0d=2.5$ ) for one hypothetical 155mm projectile with rocket motor and base-bleed unit. Maximal range is for elevation 56.1deg.

#### TRAJECTORIES FOR SEARCHING MAXIMAL RANGE

Theta0	Range	El	TOF	Vertex	Vterm	FallAng
[deg]	[m]	[mils]	[s]	[m]	[m/s]	[deg]
42.5	43873	756	106.5	12070	340	-63
45.0	45718	800	112.3	13425	346	-64
47.5	47399	844	117.9	14840	356	-64
50.0	48792	889	123.4	16307	367	-65
52.5	49776	933	128.7	17811	379	-66
55.0	50277	978	133.8	19337	390	-66
57.5	50246	1022	138.7	20868	401	-67
60.0	49631	1067	143.3	22388	412	-68
Data at maximal range						
56.1	50342	997	136.0	20013	395	-67

After the calculation of these set of trajectories program calculates and prints results for maximal range.

Table 3 – Data printed in Work space and in Graphs

IBRMResults.txt				
No.	Quantity in file	Symbol in theory	Unit	Description
<b>Standard set of data – printed always</b>				
1.	Theta0	$\theta_0$	[deg]	Initial elevation
2.	Range	$x_e$	[m]	Range
3.	El	$QE$	[mil]	Initial elevation in mils – Quadrant elevation, (division 6400)
4.	TOF	$t_e$	[s]	Time of flight
5.	Vertex MaxOrd	$h_s$	[m]	Maximal ordinate
6.	Vterm	$V_e$	[m/s]	Terminal speed
7.	FallAng	$\theta_e$	[deg]	Falling angle
8.	Time	$t$	[s]	Time
9.	Height	$h$	[m]	Height above ground
10.	VK	$V_K$	[m/s]	Velocity with respect to ground
11.	Theta	$\theta_0$	[deg]	Elevation
12.	spin	$\omega_x, p$	[rad/s]	Spin rate, axial angular speed
13.	mass	$m$	[kg]	Mass
14.	pa	$p_a$	[mbar]	Ambient atmospheric pressure
15.	pb	$p_b$	[mbar]	Base pressure – pressure on the base of projectile
16.	pc	$p_c$	[mbar]	Chamber pressure
17.	Cred	$C_{red}$	[-]	Drag reduction coefficient
18.	Cpb0	$C_{pb0}$	[-]	Base drag coefficient without influence of BB
19.	Cpb	$C_{pb}$	[-]	Base drag coefficient with influence of BB
20.	Ma	$Ma$	[-]	Flight Mach number
21.	mp, mf	$m_f(t)$	[kg]	Current mass of BB fuel
22.	mbdot mfdot	$\dot{m}_b$	[kg/s]	Mass flow rate
23.	Ab	$A_b$	[cm <sup>2</sup> ]	Burning area
24.	Inject	$I$	[-]	Base injection parameter
25.	Mj	$M_j$	[-]	Mach number in BB jet at exit area
26.	CD0	$C_{D0}$	[-]	Drag coefficient without influence of BB
27.	CD0BB	$C_{D0.BB}$	[-]	Drag coefficient with influence of BB
28.	CDb0	$C_{Db0}$	[-]	Base drag coefficient without influence of BB
29.	dDrag	$\Delta D$	[-]	Increment of drag due to influence of BB

Example of the output data is shown below.

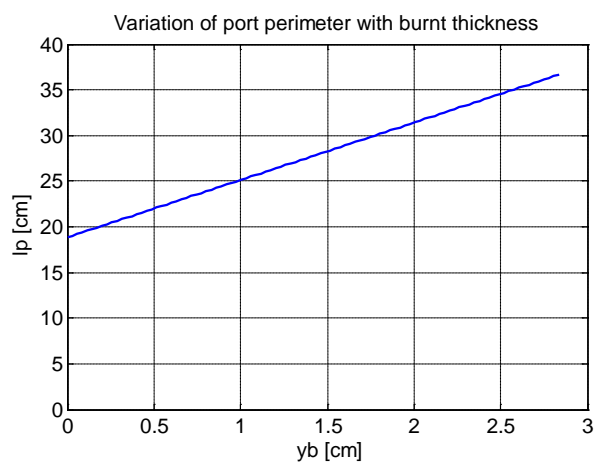
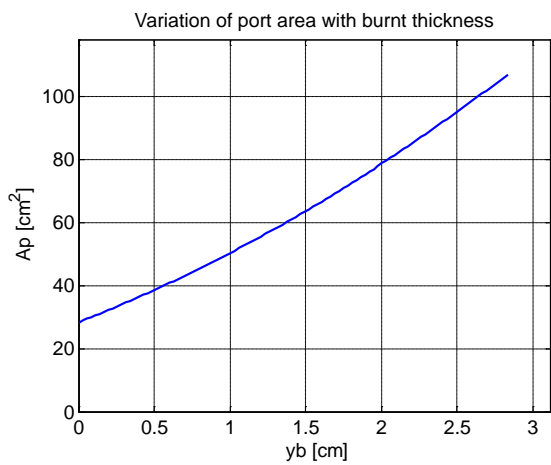
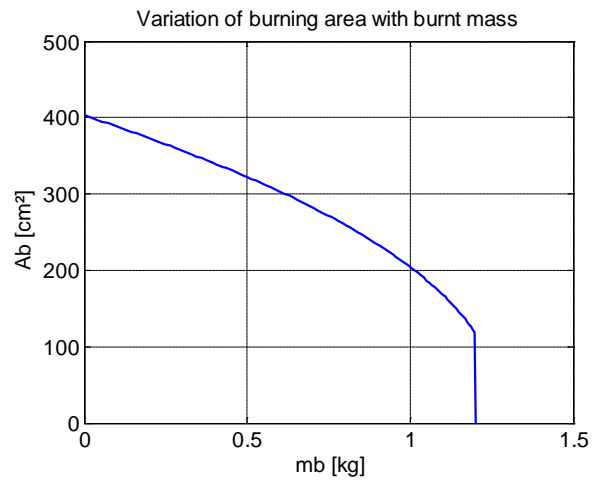
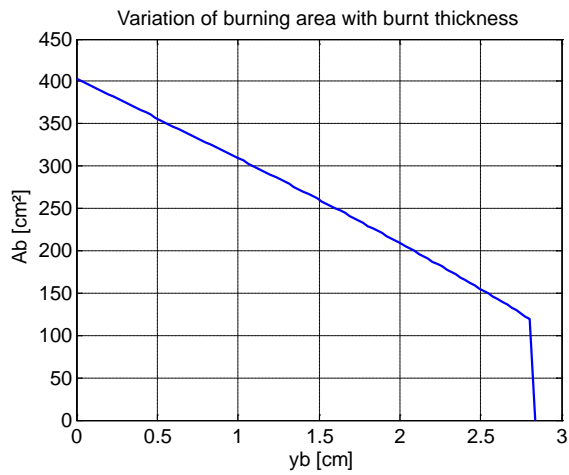
Mass of BB fuel = 1.200 kg
Mass of RM prop. = 3.800 kg

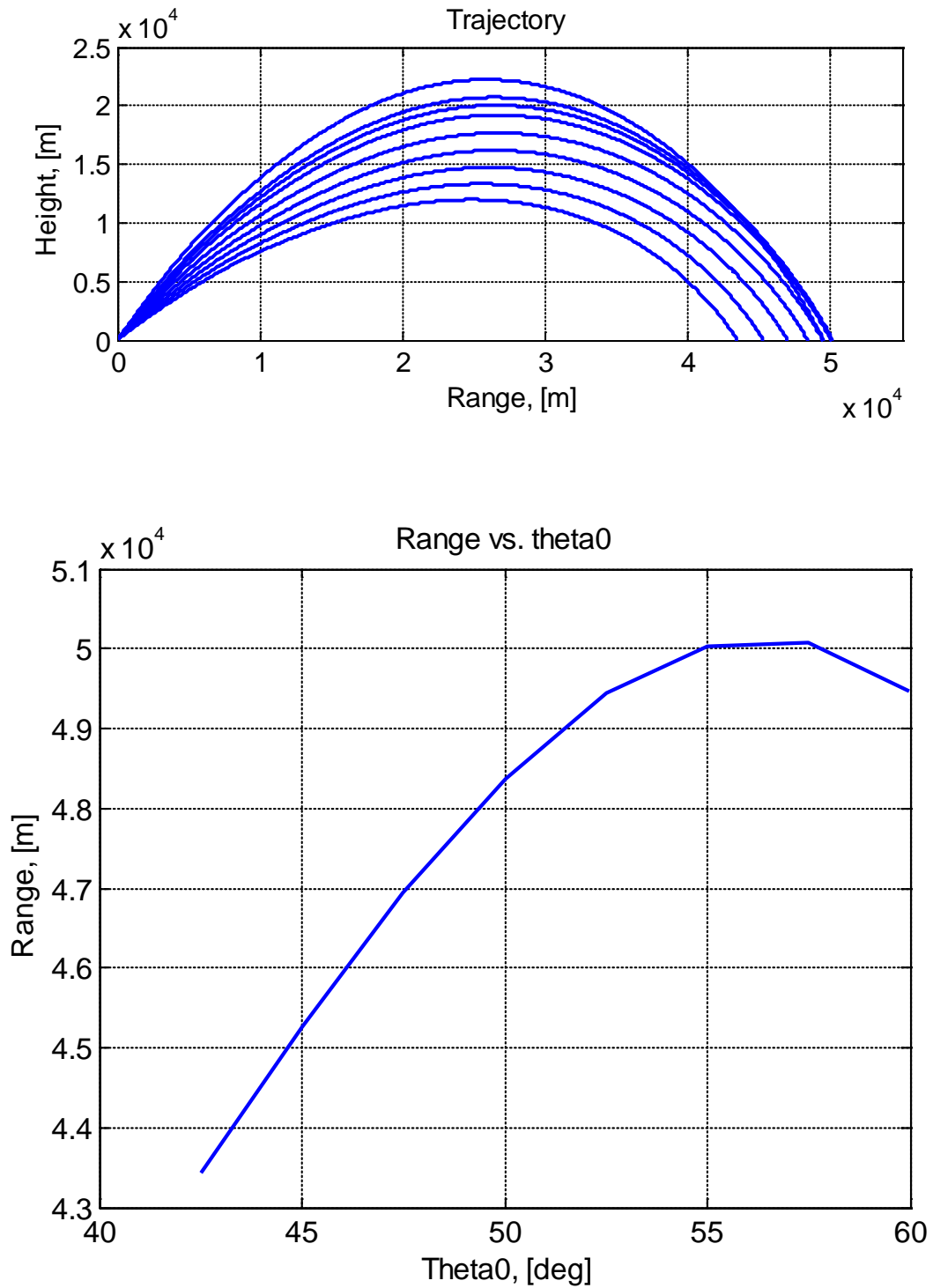
BASIC QUANTITIES OF TRAJECTORY

Table with 19 columns: Time, Range, Height, VK, Theta, spin, mass, pa, pb, pc, Cred, Cpb0, Cpb, Ma, mp, mbdot, Ab, Inject, Mj, Time. The table contains multiple rows of numerical data representing trajectory parameters over time.

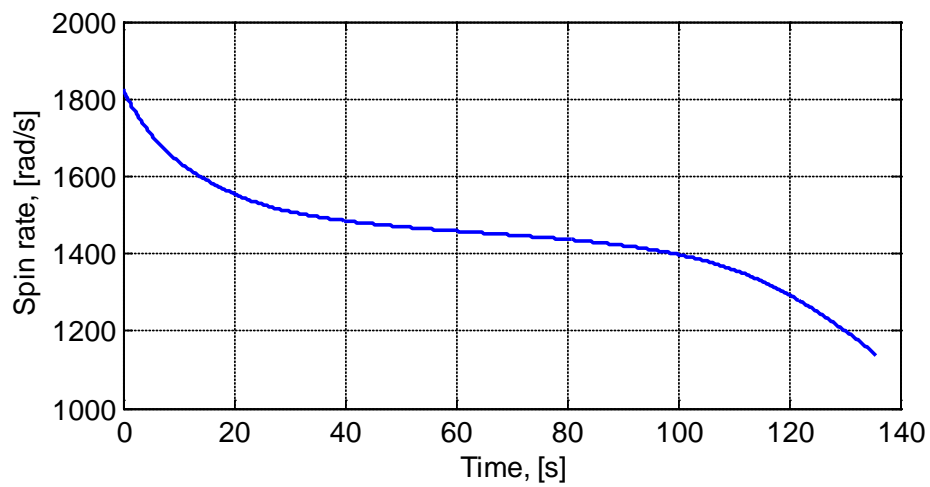
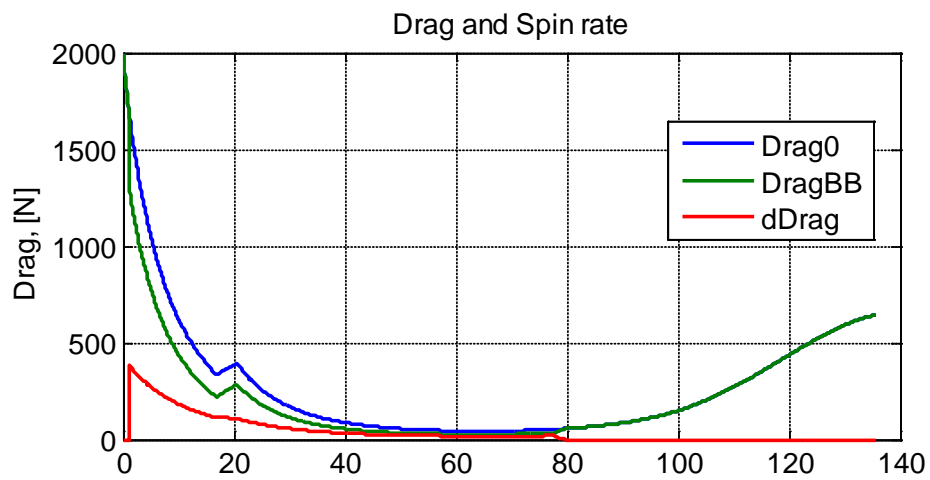
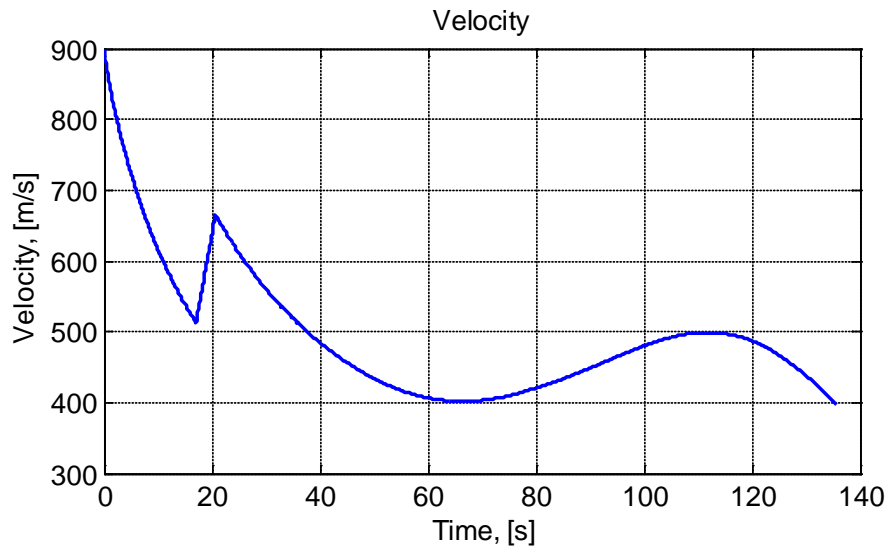
## 4.2 GRAPHS – DIAGRAMS

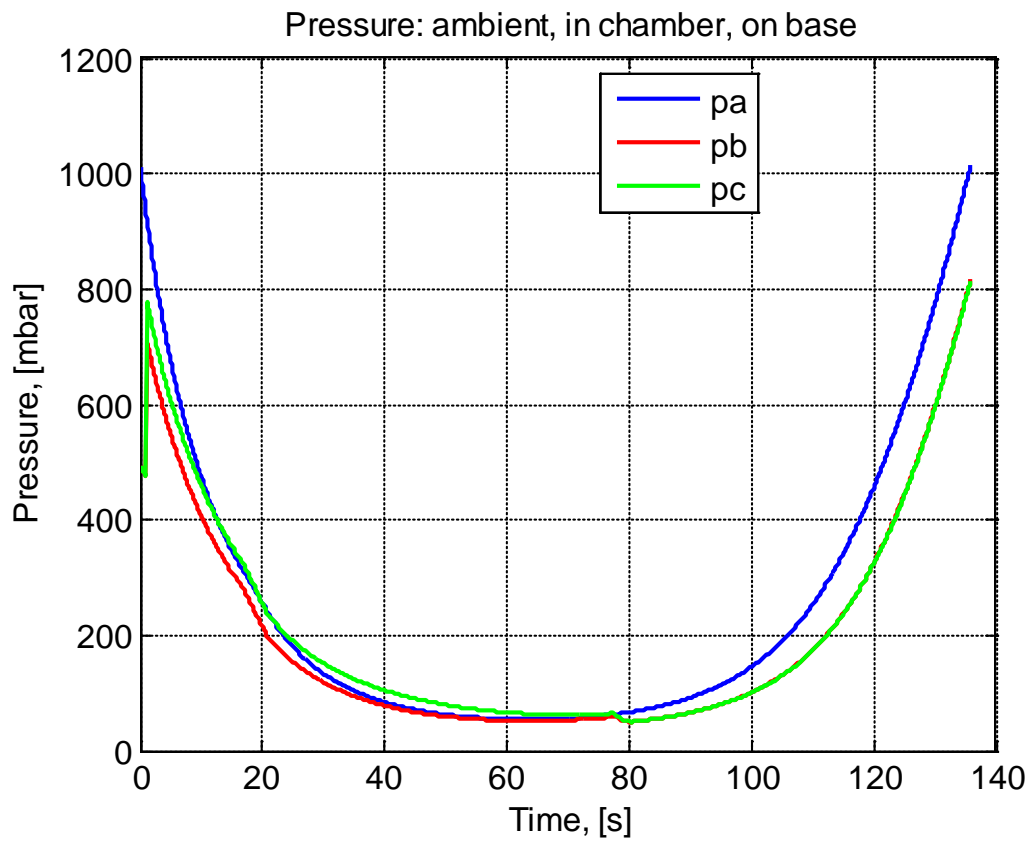
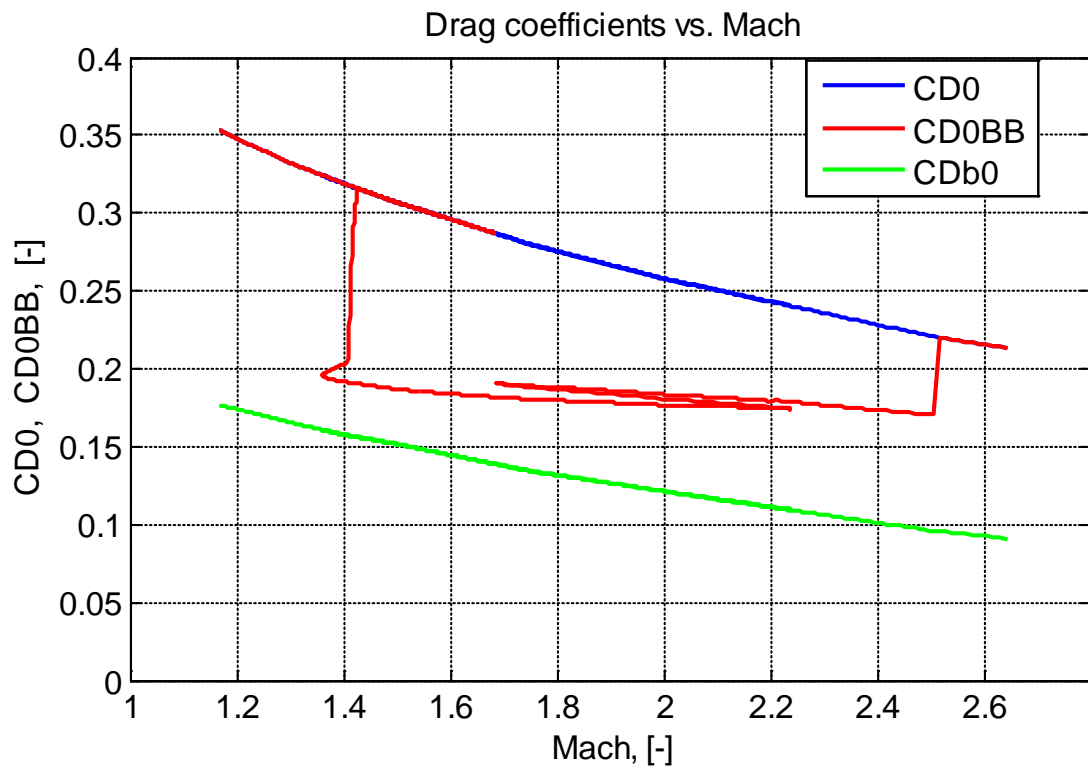
### Graphs Generated by Grain Geometry Data File

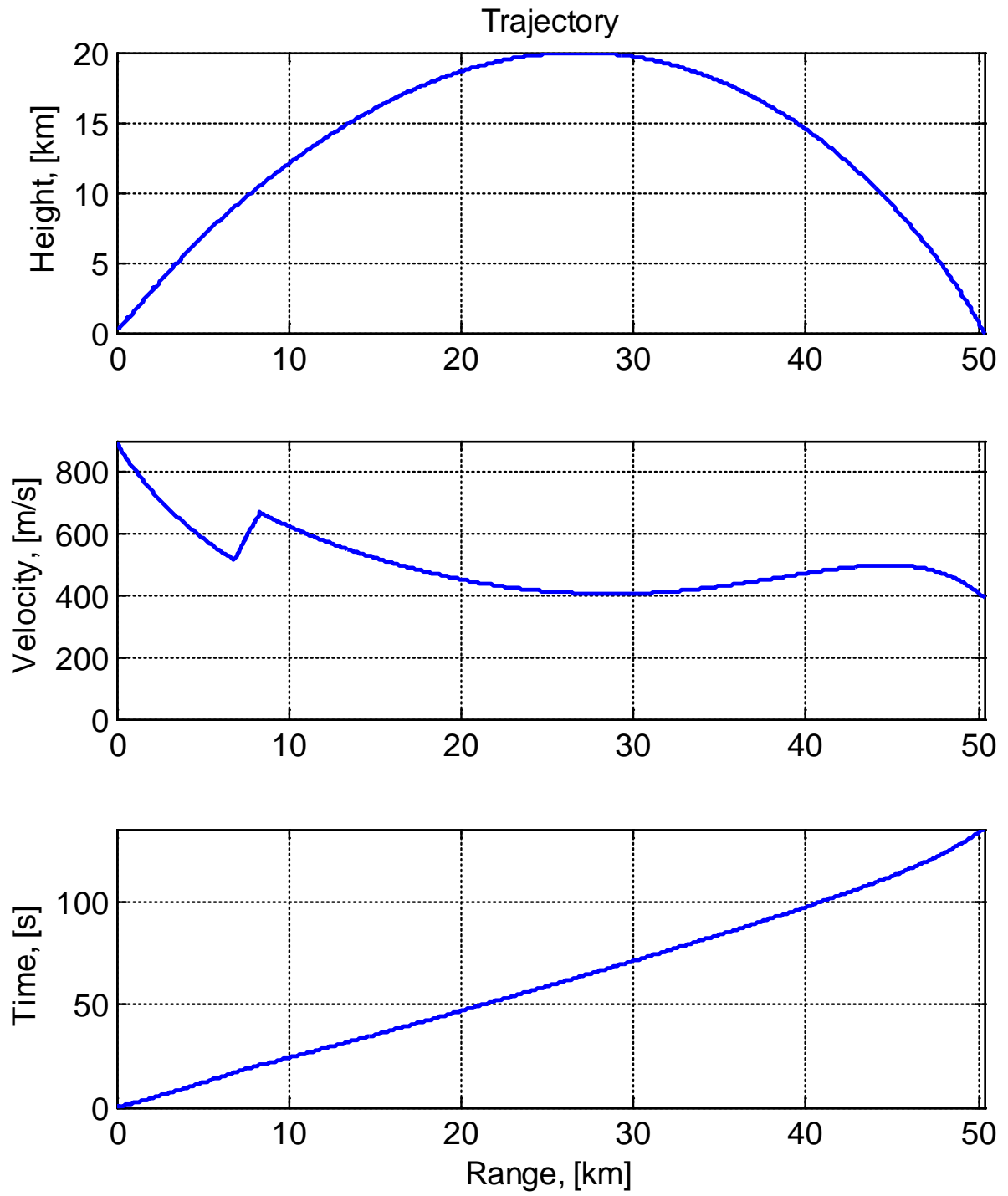


**Graphs Generated by Main program***Trajectories for Searching Maximal Range*



*Quantities on Trajectory with Maximal Range*





## Base-bleed Characteristics

